

## **AMENDMENTS TO THE SPECIFICATION**

1. Replace the paragraph beginning on line page 17, line 16 and ending on page 17, line 35 with the following amended paragraph:

At its longitudinal end which is opposite to the coupling formation 12, the tool holder 10 has a clamping formation 14 which has a clamping recess 16, which in the example shown is cylindrical and into which a shank of a tool can be introduced and clamped securely there. In the example which is shown in figure 1, the tool holder 10 serves for shrink-fit clamping purposes. The clamping formation 14 is thus heated on its outer circumferential surface 15 in the region of the clamping recess 16, so that the clamping formation expands thermally and the diameter of the clamping recess 16 increases. In this heated state, the shank of a tool is introduced into the clamping space 16, whereupon the tool holder 10 is cooled, or can cool, in the region of the clamping formation, so that between the tool holder-shank and the clamping formation 14, by virtue of the cooling-induced shrinkage of the clamping formation 14, the tool holder is secured with press-fit action in the clamping recess 16. Such tool holders are known in general from the prior art.

2. Replace the paragraph beginning on line page 23, line 28 and ending on page 24, line 2 with the following amended paragraph:

At its longitudinal end 26d, which is in the vicinity of the clamping formation, the retaining sleeve 20d has a conical inner surface 31d. The conical inner surface 31d has essentially the same inclination as the conical outer surface 15d. The conical inner surface 2831d is thus also oriented at least in the axial direction. More precisely, on account of its conicity, the surface (in the mounted state of the retaining sleeve 20d), is oriented on the one hand, in the radial direction toward the axis of rotation D and on the other hand, in the axial direction, toward the coupling formation 12d. The supporting location 24d, which is in the vicinity of the clamping formation, is thus formed by the surfaces 15d and 31d butting against one another.

3. Replace the paragraph beginning on line page 25, line 14 and ending on page 25, line 17 with the following amended paragraph:

In the embodiments which are shown in figures 5 and 6, the clamping formation 14d and ~~14e and 14d and 14e~~, respectively, is located, at least in part, in the bracing section VA.

4. Replace the paragraph beginning on line page 29, line 4 and ending on page 29, line 10 with the following amended paragraph:

Figure 11, once again, illustrates a two-part tool holder 10k, this time with the tool-holder parts 58k and 60k. In contrast to figure 10, the tool-holder parts 58k and 60k are not screw-connected to one another. Rather, the pin 49k of the tool-holder part 48k is merely plugged into the opening 47k of the tool-holder part 60k.

5. Replace the paragraph beginning on line page 37, line 5 and ending on page 37, line 11 with the following amended paragraph:

The shank section 18t is of hollow design, in order for cooling fluid to be directed through it, and at its longitudinal end 26t, it has an axially adjustable stop unit 86 ~~by means of which~~ forming an axial end stop for a tool shank which can be inserted into the clamping space 16t. Such stop units may also be provided for the other embodiments described.

6. Replace the paragraph beginning on line page 39, line 12 and ending on page 39, line 30 with the following amended paragraph:

Figure 23 shows a variant of a tool holder 10w of the shrink-fit type, this variant differing from the variant of figure 22 merely in that the friction-fit section 89w, in which the shank section 18w is oversized radially in relation to the internal diameter of the sleeve 20w, is dimensioned primarily for the frictional damping of the tool holder 10w, while the supporting location 24w, at which the sleeve 20w is supported with the prestressing force FK, is formed by a nut 95 which is screwed on to an external thread of the clamping shank 18w. Here too, the prestressing force by means of which the sleeve 20w is clamped in between its supporting locations 22w and 24w is a number of tons, for example, 10 tons. Moreover, the sleeve 20w corresponds, in terms of its form, to the sleeve 20w<sub>y</sub> in figure 22, although, in addition, in the region of the end which is directed toward the clamping formation 14w, a further damping ring 96 is provided between the sleeve 20w and the clamping shank 18w.

7. Replace the paragraph beginning on line page 46, line 1 and ending on page 46, line 18 with the following amended paragraph:

The damping elements 112 may be oversized radially relative to the inner circumference 113 and/or outer circumference 29cc, so that they are seated with radial press-fit action in the annular chamber 111. In addition, or also as an alternative, however, the radial prestressing of the damping elements 112 may also be produced by axial bracing between the two stop rings 115, 117, in that the annular shoulder 52cc, which centers the end 32cc of the sleeve 20cc on the coupling formation 12cc, adjusts the adjacent stop ring 117e by a predetermined distance towards the other stop ring 115, which is supported in the annular chamber 111. The radial bracing here is achieved by reducing the axial spacing between the stop rings 115, 117. In addition, or as an alternative, for the purpose of increasing the radial prestressing, the damping elements 112 can be driven into the tapering gap of the annular chamber 111.